

# Lecture 19 - The Magnetohydrodynamics Equations

10/31/17

🎃 Happy Halloween!

from last time...

## Deriving the MHD Equations

The MHD equations underly work in both lab physics and space & astrophysics

Ordering:  $p^+ / e^-$  masses comparable

✓ plasma velocity

$$u \sim v_t \sim c_A$$

└ Alfvén speed ( $v \ll c_A$  for  $c_A \ll c$ ,  
 $v \approx c$  for  $c_A \gg c$ )

$$c_A \sim B / \sqrt{4\pi mn}$$

↑ diverges for

collision  
rate  
↓

small  $n$ ; problematic for  
relativistic MHD (impacts  
Ampère's Law)

$$\nu \sim \Omega, \omega = v_t / L$$

$E = \omega / \nu \sim v_t^2 / c^2 \sim r_e / L \ll 1$

└  $L$  = macro scale length

└ small parameter (underlies entire derivation)

\* Ordering designed to  
make certain terms  
small so we can throw  
them out for the MHD  
equations

⇒ Use this scheme to break down our constituent equations

### The Boltzmann Equation

$$\frac{\partial f_\alpha}{\partial t} + \vec{v} \cdot \nabla f_\alpha + \left( \frac{q}{m} \right)_\alpha (\vec{E} + \frac{1}{c} \vec{v} \times \vec{B}) \cdot \frac{\partial}{\partial \vec{v}} f_\alpha = C_{\alpha\alpha} + C_{\alpha\beta}$$

Collisions

rank:  $E$        $E$       1      1      1      1      1

### Gauss' Law

✓ deviation from charge neutrality

$$\nabla \cdot \vec{E} = 4\pi e ( \int d\vec{v} f_i - \int d\vec{v} f_e )$$

rank:  $E^2$       1      1

the basis for quasineutrality → electron & ion

densities  $\sim$  equal

⇒ charge neutral @ 0<sup>th</sup> & 1<sup>st</sup> orders

\* Note: Ordering does NOT mean  $\vec{E} = 0$ , just that our scale lengths are much larger than  $\lambda_D$

### Faraday's Law

$$\frac{1}{c} \frac{\partial \vec{B}}{\partial t} + \nabla \times \vec{E} = 0$$

rank: 1 1

### Ampère's Law

$$\nabla \times \vec{B} = \frac{1}{c} \frac{\partial \vec{E}}{\partial t} + \frac{4\pi}{c} e \int d\vec{v} \vec{v} (f_i - f_e)$$

rank: E E<sup>2</sup> 1 1

L "toss forever" – not in 0<sup>th</sup> or 1<sup>st</sup> orders

\* doing this does make this not Lorentz invariant, so this is only in the non-relativistic case

Then...

Lowest Order (Rank 1): (E, E<sup>2</sup> thrown out)

#### ① Boltzmann

$$\left(\frac{q}{m}\right)_\alpha \left(\vec{E}_0 + \frac{1}{c} \vec{v} \times \vec{B}_0\right) \cdot \frac{\partial}{\partial \vec{v}} f_\alpha = \underbrace{C_{\alpha\alpha_0} + C_{\alpha\beta}}_{}$$

presence of these terms makes temperatures equal

#### ② Gauss

$$0 = n_i^\circ - n_e^\circ$$

#### ③ Faraday

$$\frac{1}{c} \frac{\partial \vec{B}_0}{\partial t} + \nabla \times \vec{E}_0 = 0$$

#### ④ Ampère

$$0 = (n_i \vec{U}_i)_0 - (n_e \vec{U}_e)_0$$

$$\Rightarrow \vec{J}_0 = 0$$

From ① → Maxwellian,  $n_e = n_i$  thus eliminating  $C_{\alpha\alpha_0}, C_{\alpha\beta}$ .

$$U_{i_0} = U_{e_0} = \vec{U}_0, T_e = T_i$$

L  $f_\alpha$  is a drifting Maxwellian

$$\left(\frac{q}{m}\right)_\alpha (\vec{E}_0 + \frac{1}{c} \vec{v} \times \vec{B}_0) \cdot \frac{\partial}{\partial \vec{v}} f_{\alpha 0} = C_{\alpha \alpha 0} + \cancel{C_{\alpha \beta 0}}$$

$$\hookrightarrow (\vec{E}_0 + \frac{1}{c} \vec{v} \times \vec{B}_0) \cdot (\vec{v} - \vec{U}_0) = 0$$

can simplify  $\frac{\partial}{\partial \vec{v}} f_{\alpha 0}$  to this b/c  $f_{\alpha 0}$  is Maxwellian

$$\vec{E}_0 \cdot (\vec{v} - \vec{U}_0) - \frac{1}{c} \vec{U}_0 \cdot \vec{v} \times \vec{B}_0 = 0$$

$\downarrow$  consolidate terms in  $\vec{v}$

$$(\vec{E}_0 + \frac{1}{c} \vec{U}_0 \times \vec{B}_0) \cdot \vec{v} = \vec{E}_0 \cdot \vec{U}_0$$

This must be valid for any  $\vec{v}$  so...

$$\hookrightarrow \vec{E}_0 + \frac{1}{c} \vec{U}_0 \times \vec{B}_0 = 0$$

\*note:  $\vec{E}_0 = 0$  in the plasma frame (the frame moving

@  $\vec{v} = \vec{U}_0$ , this is the mark of a good conductor)

•  $\vec{U}_{10}$  is the  $\vec{E}_0 \times \vec{B}_0$  drift

$$\hookrightarrow E_{0||} U_{0||} = 0 \Rightarrow E_{0||} = 0$$

$$\vec{E}_0 = -\frac{1}{c} \vec{U}_0 \times \vec{B}_0$$

$\downarrow$  from  $\vec{U}_0$  we can determine  $\vec{E}_0$

$n_0, P_0, U_0/E_0$  as yet undetermined

the moments of the Boltzmann equation

When we go to 1<sup>st</sup> order we need to deal with collisions. Therefore we will also need...

### Symmetry Properties of the Collision Operator

$$\int d\vec{v} C_{\alpha \alpha} \begin{pmatrix} 1 \\ m_\alpha \vec{v} \\ \frac{1}{2} m_\alpha v^2 \end{pmatrix} = 0$$

self-collisions (collisions within a species)  
do not change # density, momentum-, or energy-density

$$\int d\vec{v} C_{\alpha \beta} \begin{pmatrix} 1 \\ m_\alpha \vec{v} \\ \frac{1}{2} m_\alpha v^2 \end{pmatrix} = \begin{array}{l} 0 \leftarrow \# \text{density unchanged} \\ -\vec{R}_{\alpha \beta} \leftarrow \text{momentum conservation} \\ -(\frac{\partial w}{\partial t})_{\alpha \beta} \leftarrow \text{total energy unchanged} \end{array}$$

$\vec{R}_{\alpha \beta}$  = drag between species  $\alpha$  and  $\beta$

$\hookrightarrow \vec{R}_{\alpha \beta} + \vec{R}_{\beta \alpha} = 0 \Rightarrow$  momentum from  $\alpha \rightarrow \beta$  = momentum from  $\beta \rightarrow \alpha$   
(see Lecture #10 for definition)

$$\left(\frac{\partial W}{\partial t}\right)_{\alpha\beta} + \left(\frac{\partial W}{\partial t}\right)_{\beta\alpha} = 0 \Rightarrow \text{energy exchange from } \alpha \rightarrow \beta = \text{energy exchange from } \beta \rightarrow \alpha$$

NOW ↴

### First Order in E

- { Evaluate rank E terms @ 0<sup>th</sup> order
- { Evaluate rank I terms @ 1<sup>st</sup> order

To what order do we evaluate  $f_\alpha$ ? → 0<sup>th</sup>

$$\frac{\partial}{\partial t} f_{\alpha_0} + \vec{V} \cdot \nabla f_{\alpha_0} + \left(\frac{q}{m}\right)_\alpha \left[ (\vec{E} + \frac{1}{c} \vec{V} \times \vec{B}) \cdot \frac{\partial}{\partial \vec{V}} f_\alpha \right]_{1^0} = C_{\alpha\alpha} + C_{\alpha\beta},$$

evaluate @  
1<sup>st</sup> order

use symmetry to  
get rid of this

- Integrate over the Velocity (operate with  $\int d\vec{v}$ ) and use the fact that  $\frac{\partial}{\partial \vec{V}} \cdot \vec{F} = 0$  and that collisions don't create or destroy particles

Properties of the collisions:

$$\int d\vec{v} C_{\alpha\beta}(f_\alpha) = 0$$

↳ Coulomb collisions conserve particle # (from Lec. #5)

and  $f_\alpha \rightarrow 0$  as  $V \rightarrow \infty$

$$\underbrace{\frac{\partial}{\partial t} \int d\vec{v} f_{\alpha_0}}_{n_{\alpha_0}} + \underbrace{\nabla \cdot \int d\vec{v} \vec{V} f_{\alpha_0}}_{n_{\alpha_0} \vec{U}_0} + \left(\frac{q}{m}\right)_\alpha \underbrace{\int d\vec{v} (\vec{E} + \frac{1}{c} \vec{V} \times \vec{B}) \cdot \frac{\partial}{\partial \vec{V}} f_\alpha}_{\frac{\partial}{\partial \vec{V}} \cdot \vec{F} = 0} = \underbrace{\int d\vec{v} (C_{\alpha\alpha} + C_{\alpha\beta})}_0$$

$$\begin{aligned} \frac{\partial}{\partial \vec{V}} \cdot (\vec{E} + \vec{V} \times \vec{B}) &= 0 + \frac{\partial}{\partial \vec{V}} \cdot (\vec{V} \times \vec{B}) \\ &= \vec{B} \cdot \underbrace{(\frac{\partial}{\partial \vec{V}} \times \vec{V})}_0 = 0 \end{aligned}$$

$$\Rightarrow \frac{\partial n}{\partial t} + \nabla \cdot n \vec{U} = 0$$

The Continuity Equation

\* implied sub<sub>0</sub> unless otherwise written from here on out

### NOW: Momentum Equation

Operate with  $\int d\vec{v} \vec{V}$  — multiply by  $\vec{V}$  and integrate

→ Note:  $\vec{V}$  is an independent variable and so passes

through  $\nabla$ ,  $\frac{\partial}{\partial t}$  operators (and  $\int d\vec{v} f_{\alpha_0} = n_{\alpha_0}$ )

$$\underbrace{\frac{\partial}{\partial t} \int d\vec{v} f_{\alpha_0} \vec{v}}_{n_{\alpha} \vec{u}} + \nabla \cdot \int d\vec{v} \vec{v} \vec{v} f_{\alpha_0} + \int d\vec{v} \vec{v} \frac{\vec{F}}{m_{\alpha}} \cdot \frac{\partial}{\partial \vec{v}} f_{\alpha_0} = \int d\vec{v} \vec{v} (C_{\alpha\alpha_1} + C_{\alpha\beta_1})$$

$$= \frac{-1}{m_{\alpha}} \vec{R}_{\alpha\beta_1}$$

$$\int d\vec{v} f_{\alpha} \vec{v} = n_{\alpha} \vec{u}$$

where  $\vec{R}_{\alpha\alpha} = 0$ ; i.e., no drag within a species

local momentum	flux of momentum	change of momentum from $\vec{E}$ -field
$\frac{\partial}{\partial t} n_{\alpha} \vec{u}$	$\nabla \cdot \int d\vec{v} \vec{v} \vec{v} f_{\alpha_0}$	$-\frac{q_{\alpha}}{m_{\alpha}} n_{\alpha} (\vec{E} + \frac{1}{c} \vec{u} \times \vec{B})$

$$= \frac{-1}{m_{\alpha}} \vec{R}_{\alpha\beta_1}$$

We can extract average velocity from  $\nabla \cdot \int d\vec{v} \vec{v} \vec{v} f_{\alpha_0}$ .

Let  $\vec{v}' \equiv \vec{u} + \vec{v}'$

note that  $\int d\vec{v}' v' f_{\alpha} = 0$

$$\nabla \cdot \int d\vec{v} \vec{v} \vec{v} f_{\alpha} = \nabla \cdot (n_{\alpha} \vec{u} \vec{u}) + \nabla \cdot \int d\vec{v}' \vec{v}' \vec{v}' f_{\alpha}(\vec{v}')$$

Define the pressure tensor

$$\bar{\bar{P}}_{\alpha} = m_{\alpha} \int d\vec{v}' \vec{v}' \vec{v}' f_{\alpha}$$

Then, rearranging the above equation

$$\frac{\partial}{\partial t} n_{\alpha} \vec{u} + \nabla \cdot \int d\vec{v} \vec{v} \vec{v} f_{\alpha} = \left( \frac{q}{m} \right)_{\alpha} n_{\alpha} (\vec{E} + \frac{1}{c} \vec{u} \times \vec{B}) - \frac{1}{m_{\alpha}} \vec{R}_{\alpha\beta_1}$$

$$m_{\alpha} \left( \frac{\partial}{\partial t} n_{\alpha} \vec{u} + \nabla \cdot \int d\vec{v} \vec{v} \vec{v} f_{\alpha} \right) = q_{\alpha} n_{\alpha} (\vec{E} + \frac{1}{c} \vec{u} \times \vec{B}) - \vec{R}_{\alpha\beta_1}$$

plug in value defined above

$$m_{\alpha} \left[ \frac{\partial}{\partial t} n_{\alpha} \vec{u} + \nabla \cdot (n_{\alpha} \vec{u} \vec{u}) + \nabla \cdot \int d\vec{v}' \vec{v}' \vec{v}' f_{\alpha}(\vec{v}') \right] = q_{\alpha} n_{\alpha} (\vec{E} + \frac{1}{c} \vec{u} \times \vec{B}) - \vec{R}_{\alpha\beta_1}$$

$$m_{\alpha} \left[ \frac{\partial}{\partial t} n_{\alpha} \vec{u} + \nabla \cdot (n_{\alpha} \vec{u} \vec{u}) \right] + \nabla \cdot \underbrace{m_{\alpha} \int d\vec{v}' \vec{v}' \vec{v}' f_{\alpha}(\vec{v}')}_{\bar{\bar{P}}_{\alpha}} = q_{\alpha} n_{\alpha} (\vec{E} + \frac{1}{c} \vec{u} \times \vec{B}) - \vec{R}_{\alpha\beta_1}$$

$$m_{\alpha} \left[ \frac{\partial}{\partial t} n_{\alpha} \vec{u} + \nabla \cdot (n_{\alpha} \vec{u} \vec{u}) \right] = q_{\alpha} n_{\alpha} (\vec{E} + \frac{1}{c} \vec{u} \times \vec{B}) - \nabla \cdot \bar{\bar{P}}_{\alpha} - \vec{R}_{\alpha\beta_1}$$

use the continuity equation,  $\frac{\partial}{\partial t} n_{\alpha} + \nabla \cdot n_{\alpha} \vec{u} = 0$ ,

to extract  $n_{\alpha}$  on this LHS

$$n_{\alpha} m_{\alpha} \left[ \frac{\partial}{\partial t} \vec{u} + \vec{u} \cdot \nabla \vec{u} \right] = n_{\alpha} q_{\alpha} (\vec{E} + \frac{1}{c} \vec{u} \times \vec{B}) - \nabla \cdot \bar{\bar{P}}_{\alpha} - \vec{R}_{\alpha\beta_1}$$

$$\frac{d}{dt} = \frac{\partial}{\partial t} + \vec{u} \cdot \nabla$$



$$n_\alpha m_\alpha \frac{d}{dt} \vec{U} = n_\alpha q_\alpha (\vec{E} + \frac{1}{c} \vec{U} \times \vec{B}) - \underbrace{\nabla \cdot \vec{P}_\alpha}_{\nabla \cdot \vec{P}_\alpha = \nabla P_\alpha + \nabla \cdot \overline{\delta P_\alpha} \approx \nabla P_\alpha} - \vec{R}_{\alpha\beta},$$

Must break this down  
into rank 1 & rank E

$$\nabla \cdot \vec{P}_\alpha = \nabla P_\alpha + \nabla \cdot \overline{\delta P_\alpha} \approx \nabla P_\alpha$$

viscous stress  
 $\sim 1/\nu \rightarrow$  small

$$n_\alpha m_\alpha \frac{d}{dt} \vec{U} = -\nabla P_\alpha - \vec{R}_{\alpha\beta} + n_\alpha q_\alpha (\vec{E}_i + \frac{1}{c} \vec{U} \times \vec{B}_i) + q_\alpha (n_\alpha \vec{E}_0 + \frac{1}{c} (n \vec{U})_\alpha \times \vec{B}_0)$$

take  $\vec{E}, \vec{B}$  1<sup>st</sup> order; all other terms in 0<sup>th</sup> order

$\frac{1}{c} q_\alpha \cdot$  first-order current,  $\vec{J}_i$

↓ sum over species  $\alpha$  and  $\beta$  ↓

$$n_\alpha = n_{i\alpha}, 0^{\text{th}} \text{ O Ampère's Law}$$

$$n_\alpha (m_\alpha + m_\beta) \frac{d}{dt} \vec{U} = -\nabla (P_\alpha + P_\beta) - (\vec{R}_{\alpha\beta} + \vec{R}_{\beta\alpha}) + n_{i\alpha} (-e + e) (\vec{E}_i + \frac{1}{c} \vec{U} \times \vec{B}_i) + (-e + e) (n_\alpha \vec{E}_0) + \frac{1}{c} \vec{J}_i \times \vec{B}_0$$

0: symmetry properties

$\vec{J}_i = e(n \vec{U})_i - e(n \vec{U})_e$

$$n(m_\alpha + m_\beta) \frac{d}{dt} \vec{U} = -\nabla (P_\alpha + P_\beta) + \frac{1}{c} \vec{J}_i \times \vec{B}$$

\* Define:

$$\rho = (m_\alpha + m_\beta)n, \text{ total } 0^{\text{th}} \text{ order density}$$

$$P = P_\alpha + P_\beta, \text{ total pressure}$$

↓ plugging in ↓

$$\rho \frac{d}{dt} \vec{U} = -\nabla P + \frac{1}{c} \vec{J}_i \times \vec{B}$$

The Momentum  
Equation

$$\nabla \times \vec{B} = \frac{4\pi}{c} \vec{J}_i$$

⇒ We now know  $n_0, U_0/E_0$ !

Only need an expression for the pressure now

### Pressure Equation

Operate with  $\int d\vec{v} v^2$  - multiply by  $\frac{1}{2} m v^2$  and integrate

$$\begin{aligned} \frac{\partial}{\partial t} \int d\vec{v} \frac{m_\alpha v^2}{2} f_\alpha + \nabla \cdot \left[ \int d\vec{v} \frac{m_\alpha v^2}{2} \vec{v} f_\alpha \right] + \frac{q_\alpha}{m_\alpha} \int d\vec{v} \frac{m_\alpha v^2}{2} \frac{\partial}{\partial \vec{v}} \cdot (\vec{E} + \frac{1}{c} \vec{v} \times \vec{B}) f_\alpha \\ = \int d\vec{v} \frac{m_\alpha v^2}{2} (C_{\alpha\alpha} + C_{\alpha\beta}) \end{aligned}$$

Recall  $f_\alpha$  is a drifting Maxwellian

$$\vec{v}' = \vec{v} - \vec{U} \rightarrow \vec{v} = \vec{v}' + \vec{U}$$

$$f_\alpha = \frac{n_\alpha}{(2\pi T_\alpha/m_\alpha)^{3/2}} e^{-(\vec{v}' - \vec{U})^2 m_\alpha / 2T_\alpha}$$

Plugging in term-by-term:

$$\int d\vec{v} \frac{m_\alpha v^2}{2} f_\alpha = \underbrace{\frac{m_\alpha U^2}{2} \int d\vec{v} f_\alpha}_{n} + \underbrace{\frac{m_\alpha}{2} \int d\vec{v}' v'^2 f_\alpha}_{3nT_\alpha/m_\alpha} - \text{cross-terms go away; odd in } \vec{v}'=0$$

$$= \frac{1}{2} m_\alpha U^2 n + \frac{3}{2} n T_\alpha$$

$$\begin{aligned} \int d\vec{v} \frac{m_\alpha v^2}{2} \vec{v} f_\alpha &= \int d\vec{v} \frac{m_\alpha (\vec{v}' + \vec{U})^2}{2} (\vec{v}' + \vec{U}) f_\alpha \\ &= \underbrace{\frac{m_\alpha U^2}{2} \vec{U} \int d\vec{v} f_\alpha}_n + \underbrace{\int d\vec{v}' \frac{m_\alpha v'^2}{2} \vec{v}' f_\alpha}_{\equiv \bar{Q}_\alpha} + \underbrace{\frac{m_\alpha}{2} \vec{U} \int d\vec{v}' v'^2 f_\alpha}_{3nT_\alpha/m_\alpha} \\ &\quad + \underbrace{\int d\vec{v}' \frac{m_\alpha}{2} 2\vec{v}' \cdot \vec{U} \vec{v}' f_\alpha}_{} \end{aligned}$$

only survives if two components of  $\vec{v}'$  are the same  
 ↳ lose two degrees of freedom

$$\begin{aligned} \int d\vec{v}' v'^2 f_\alpha - 2 \text{D.O.F.} &= n T_\alpha / m_\alpha \\ = \frac{1}{2} n m_\alpha U^2 \vec{U} + \bar{Q}_\alpha + \frac{3}{2} n T_\alpha \vec{U} + n T_\alpha \vec{U} \\ &\quad \text{heat flux} \\ = \left( \frac{1}{2} n m_\alpha U^2 + \frac{3}{2} n T_\alpha \right) \vec{U} + \bar{Q}_\alpha + n T_\alpha \vec{U} \end{aligned}$$

$$\bullet q_\alpha \int d\vec{v} \underbrace{\frac{v^2}{2} \frac{\partial}{\partial v}}_{-\vec{v}} \cdot (\vec{E} + \frac{1}{c} \vec{v} \times \vec{B}) f_\alpha = - q_\alpha \int d\vec{v} \vec{v} \cdot (\vec{E} + \frac{1}{c} \vec{v} \times \vec{B}) f_\alpha \xrightarrow{0}$$

motion of fluid in direction of field

$$= -q_\alpha \vec{E} \underbrace{\int d\vec{v} \vec{v} f_\alpha}_{\vec{U} n_\alpha} = -q_\alpha \vec{E} \cdot \vec{U} n_\alpha$$

must break this down into rank 1 and rank E

$$= -q_\alpha [n \vec{U} \cdot \vec{E}_0 + \underbrace{(n \vec{U})_{\alpha_i} \cdot \vec{E}_0}_{\gamma q_\alpha \vec{J}_i}]$$



Putting it all together:

$$\frac{\partial}{\partial t} \left( \frac{1}{2} m_\alpha u^2 n + \frac{3}{2} n T_\alpha \right) + \nabla \cdot \left( \frac{1}{2} n m_\alpha u^2 + \frac{3}{2} n T_\alpha \right) \vec{u} + \nabla \cdot \vec{Q}_\alpha + \nabla \cdot (n T_\alpha \vec{u})$$

usually assumed small

$$= q_\alpha \left[ n \vec{u} \cdot \vec{E}_i + \frac{\vec{J}_i \cdot \vec{E}_o}{q_\alpha} \right] + \underbrace{\sum_\beta \int d\vec{v} \frac{m_\alpha v^2}{2} (C_{\alpha\alpha} + C_{\alpha\beta})}_{= - \left( \frac{\partial w}{\partial t} \right)_\alpha^\circ - \left( \frac{\partial w}{\partial t} \right)_{\alpha\beta}} \quad \text{from C symmetry}$$

$$\frac{\partial}{\partial t} \left( \frac{1}{2} m_\alpha u^2 + \frac{3}{2} P_\alpha \right) + \nabla \cdot \left( \frac{1}{2} n m_\alpha u^2 + \frac{3}{2} P_\alpha \right) \vec{u} + \nabla \cdot (P_\alpha \vec{u})$$

$$= q_\alpha n \vec{u} \cdot \vec{E}_i + \vec{J}_i \cdot \vec{E}_o - \left( \frac{\partial w}{\partial t} \right)_{\alpha\beta}$$

↓ sum over species  $\alpha$  and  $\beta$  ↓

$$\begin{array}{c} \text{total pressure, } P \\ \hline \end{array}$$

$$\frac{\partial}{\partial t} \left[ \frac{1}{2} (m_\alpha + m_\beta) n u^2 + \frac{3}{2} (P_\alpha + P_\beta) \right] + \nabla \cdot \left[ \frac{1}{2} n (m_\alpha + m_\beta) u^2 + \frac{3}{2} (P_\alpha + P_\beta) \right] \vec{u} + \nabla \cdot [(P_\alpha + P_\beta) \vec{u}]$$

$$\text{total mass density, } \rho$$

$$= (-e + e) n \vec{u} \cdot \vec{E}_i + \vec{J}_i \cdot \vec{E}_o - \left[ \left( \frac{\partial w}{\partial t} \right)_{\alpha\beta} + \left( \frac{\partial w}{\partial t} \right)_{\beta\alpha} \right] \rightarrow 0; \text{ conservation of energy}$$

$$\Rightarrow \frac{\partial}{\partial t} \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) + \nabla \cdot \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) \vec{u} + \nabla \cdot (P \vec{u})$$

$$= \vec{J}_i \cdot \vec{E} = -\frac{1}{c} \vec{J}_i \cdot (\vec{u} \times \vec{B})$$

l plug in  $\vec{E}_o = -\frac{1}{c} \vec{u} \times \vec{B}$

$$= \vec{u} \cdot \frac{1}{c} (\vec{J}_i \times \vec{B})$$

↑ flipping order flips sign:  $\vec{A} \cdot \vec{B} \times \vec{C} = -\vec{B} \cdot (\vec{A} \times \vec{C}) = \vec{C} \cdot (\vec{A} \times \vec{B})$

permutations  
do not  
change sign

then from the momentum equation

$$\frac{1}{c} \vec{J}_i \times \vec{B} = \rho \frac{d}{dt} \vec{u} + \nabla P$$

↓ plugging in ↓

$$\frac{\partial}{\partial t} \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) + \nabla \cdot \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) \vec{u} + \nabla \cdot (P \vec{u}) = \vec{u} \cdot \left[ \rho \frac{d}{dt} \vec{u} + \nabla P \right]$$

### The Energy Equation

\*  $\vec{B}$  has completely dropped out! This yields the same result as before with our fluid eqns., even with a  $\vec{B}$ -field present!

KLE

$$\frac{\partial}{\partial t} \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) + \nabla \cdot \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) \vec{u} + \nabla \cdot (\rho \vec{u}) = \vec{u} \cdot [\rho \frac{d}{dt} \vec{u} + \nabla P]$$

$$= \vec{u} \cdot \nabla P + \underbrace{\rho \vec{u} \cdot \frac{d}{dt} \vec{u}}_{= \rho \frac{d u^2}{dt} / 2}$$

$\uparrow \frac{d}{dt} = \frac{\partial}{\partial t} + \vec{u} \cdot \nabla$

$$\frac{1}{2} u^2 \frac{\partial \rho}{\partial t} + \frac{\partial}{\partial t} \left( \frac{3}{2} P \right) + \vec{u} \cdot \nabla \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) + \left( \frac{1}{2} \rho u^2 + \frac{3}{2} P \right) \nabla \cdot \vec{u} + \vec{u} \cdot \nabla P$$

$$+ P \nabla \cdot \vec{u} = \vec{u} \cdot \nabla P + \cancel{\rho \left( \frac{\partial}{\partial t} + \vec{u} \cdot \nabla \right) \frac{u^2}{2}}$$

$$\cancel{\rho \left( \frac{\partial u^2}{\partial t} / 2 \right)} + \cancel{\rho \left( \vec{u} \cdot \nabla \right) \frac{u^2}{2}}$$

$\circ \frac{\partial}{\partial t}$  does not operate on  $u^2$  as seen  
in first term of LHS

$$\frac{1}{2} u^2 \left( \frac{\partial \rho}{\partial t} + (\vec{u} \cdot \nabla) \rho + \rho (\nabla \cdot \vec{u}) \right) + \frac{\partial}{\partial t} \left( \frac{3}{2} P \right) + \vec{u} \cdot \nabla \left( \frac{3}{2} P \right) + \left( \frac{3}{2} P \right) \nabla \cdot \vec{u}$$

$$+ P \nabla \cdot \vec{u} = \rho (\vec{u} \cdot \nabla) \frac{u^2}{2}$$

$$= \frac{1}{2} u^2 (\vec{u} \cdot \nabla) \rho$$

$\hookrightarrow$  move to LHS, expand  $\frac{\partial \rho}{\partial t}$

$$-\frac{1}{2} u^2 [\cancel{\rho (\nabla \cdot \vec{u})} + \cancel{(\vec{u} \cdot \nabla) \rho}] + \frac{\partial}{\partial t} \left( \frac{3}{2} P \right) + \frac{1}{2} u^2 (\vec{u} \cdot \nabla) \rho + \frac{3}{2} \vec{u} \cdot \nabla P + \left( \frac{1}{2} \rho u^2 + \frac{5}{2} P \right) \nabla \cdot \vec{u} = 0$$

$$\underbrace{\frac{\partial}{\partial t} \left( \frac{3}{2} P \right) + \frac{3}{2} \vec{u} \cdot \nabla P + \left( \frac{5}{2} P \right) \nabla \cdot \vec{u}}_{\frac{d}{dt} = \frac{\partial}{\partial t} + \vec{u} \cdot \nabla} = 0$$

$$\Rightarrow \frac{d}{dt} P + \frac{5}{3} P \nabla \cdot \vec{u} = 0$$

Summarizing...

### \*The Magnetohydrodynamics Equations\*

→ Pressure/Energy Equation:

$$\frac{d}{dt} P + \frac{5}{3} P \nabla \cdot \vec{u} = 0 \quad \text{evolves } P$$

→ Continuity Equation:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \vec{u} = 0 \quad \text{evolves mass density}$$

$\hookrightarrow \rho$  varying;  $\rho = (m_i + m_e) n$

→ Momentum Equation:

$$\rho \frac{d}{dt} \vec{U} = -\nabla P + \frac{1}{c} \vec{J} \times \vec{B} \quad \text{evolves } \vec{U}$$

↪  $\vec{J} = \vec{J}_i$ , but we drop the index

$$= -\nabla \left( P + \frac{B^2}{8\pi} \right) + \frac{1}{4\pi} (\vec{B} \cdot \nabla) \vec{B}$$

$$\nabla \times \vec{B} = \frac{4\pi}{c} \vec{J}$$

$$\nabla \cdot \vec{B} = 0$$

$$\vec{E} = -\frac{1}{c} \vec{U} \times \vec{B}$$

\*Note: take  $\vec{E} \cdot \vec{B}$

$$\hookrightarrow E_{||} = \frac{\vec{E} \cdot \vec{B}}{B} = 0 \Rightarrow \text{no parallel electric field in traditional MHD model}$$

$$\frac{1}{c} \frac{d}{dt} \vec{B} + \nabla \times \vec{E} = 0 \quad \text{evolves } \vec{B}$$

NOW: Using the MHD equations

↪ starting with "ground zero"

### Ideal MHD Equilibria

In exploring the stability & dynamics of magnetized plasma, it is useful to start with states that are time stationary so that they are in a state of equilibrium. We will discuss several examples of such states.

↪ for simplicity, we will limit this discussion to situations without flow, although in many cases equilibria with flow can also be constructed

- spatial - but no time dependence  
(plasma in a state of equilibrium)
- no waves
- no instabilities
- $\vec{U} = 0$   
(no flow)

Stationary Systems  
→ want to know  
what these look like



The basic MHD equations:

$$\textcircled{1} \quad 0 = -\nabla P + \frac{1}{c} \vec{J} \times \vec{B}$$

$$\vec{J} = \frac{c}{4\pi} (\nabla \times \vec{B})$$

$$= -\nabla P + \frac{1}{c} \underbrace{\frac{c}{4\pi} (\nabla \times \vec{B}) \times \vec{B}}_{= -\frac{1}{2} \nabla B^2 + \vec{B} \cdot \nabla \vec{B}}$$

$$= -\nabla \left( P + \frac{B^2}{8\pi} \right) + \frac{1}{4\pi} (\vec{B} \cdot \nabla) \vec{B}$$

$$\textcircled{2} \quad \vec{E} = 0$$

$$\textcircled{3} \quad \nabla \cdot \vec{B} = 0$$

$$\textcircled{4} \quad \nabla \times \vec{B} = \frac{4\pi}{c} \vec{J}$$

What do these tell us?

- Take  $\vec{B} \cdot$  eqn. ①  $\rightarrow \vec{B} \cdot \nabla P = 0$

$\Rightarrow$  Pressure must be constant along  $\vec{B}$ -field lines

\* non-constant pressure generates a sound wave that smooths/  
relaxes parallel pressure gradients out!

- Take  $\nabla \cdot$  eqn. ④  $\rightarrow \nabla \cdot (\nabla \times \vec{B}) = 0 = \nabla \cdot \left( \frac{4\pi}{c} \vec{J} \right)$

$$\nabla \cdot \vec{J} = 0$$

$\Rightarrow$  There is no build-up of charge

\* charge build-up would produce an  $\vec{E} \neq 0$ , and since  $\vec{E} = -\frac{1}{c} \vec{u} \times \vec{B}$ ,  
flows would be generated, which we have forbidden

Consider some examples...

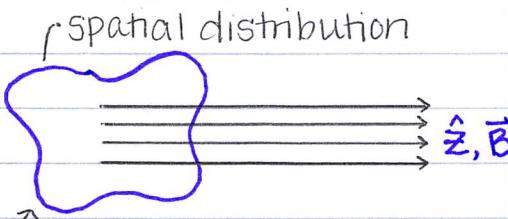
Case I:  $(\vec{B} \cdot \nabla) \vec{B} = 0$

means we have straight field lines  
( $\hat{b}$  and  $|\vec{B}|$  unchanging)

$\Rightarrow \nabla \left( P + \frac{B^2}{8\pi} \right) = 0$ , Total pressure must be a constant

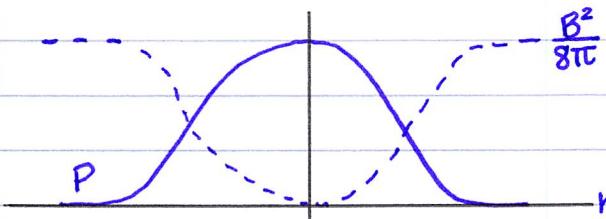
plasma pressure      magnetic pressure

How does this impact the spatial distributions  
of  $P$  and  $B$  in our system?



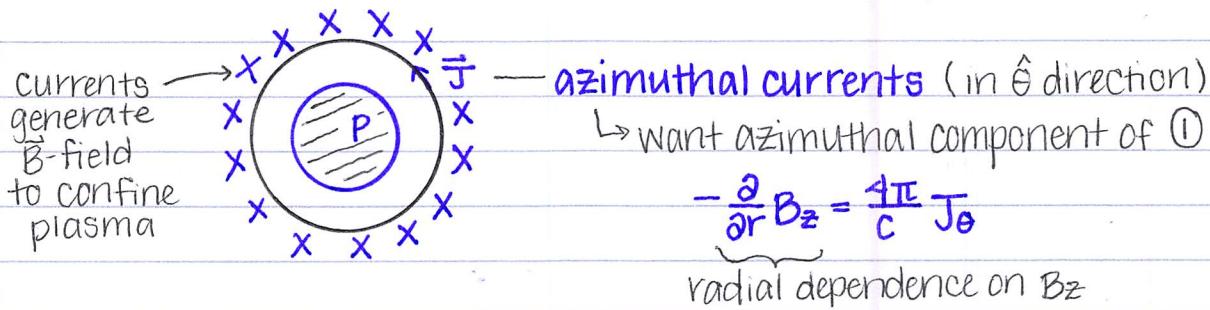
You can have any spatial distribution of  $P$  &  $B$  that you want as long as  $P + \frac{B^2}{8\pi} = \text{constant}$

- This is not a trivial state ↗ e.g., in 1-D:



\*this is a localized plasma system supported by a  $\vec{B}$ -field on the outside

Confinement experiments with such equilibria are called  $\theta$ -pinches



Case II:  $(\vec{B} \cdot \nabla) \vec{B} \neq 0$

↗ we now have curved field lines

Simple case —

$\vec{B} = B_\theta \hat{\theta}$ ; azimuthal  $\vec{B}$ -field only  
then

$$(\vec{B} \cdot \nabla) \vec{B} = [(\hat{b} |\vec{B}|) \cdot \nabla] (\hat{b} |\vec{B}|)$$

$$\hat{b} = \frac{\vec{B}}{|\vec{B}|}$$

$$= B^2 (\hat{b} \cdot \nabla) \hat{b} = B^2 \vec{K}$$

$$= \frac{B_\theta}{r} \frac{\partial}{\partial \theta} B_\theta \hat{\theta}$$

recall:  $\vec{K} = \hat{b} \cdot \nabla \hat{b}$ , the curvature of  $\vec{B}$

↓ take  $B_\theta$  to be independent of  $\theta$  ↓

$$(\vec{B} \cdot \nabla) \vec{B} = \frac{B_0}{r} B_0 \underbrace{\frac{\partial}{\partial \theta} \hat{\theta}}_{-\hat{r}} = -\frac{B_0^2}{r} \hat{r}$$

compare back to  $B^2 \vec{R}$

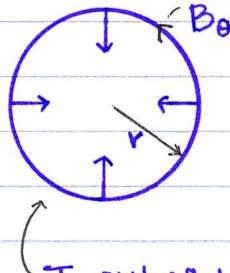
where  $K \propto 1/R_c \Rightarrow R_c = r$

↳ radius of curvature

eqn. ① becomes

$$\frac{\partial}{\partial r} \left( P + \frac{B_0^2}{8\pi} \right) + \underbrace{\frac{B_0^2}{r}}_{\text{magnetic tension}} = 0$$

magnetic tension



↳ Tension force from the  $\vec{B}$ -field can help balance variations in the total plasma pressure (that may not be uniform in space)  
→ Field can confine a plasma!

$J_z$  out of the page — current along  $\hat{z}$  is a  $z$ -pinch  
 $(\nabla \times (B_\theta \hat{\theta}))_z = \frac{4\pi}{c} J_z$

↳ curl of  $\hat{\theta} \neq 0$ ! → write  $\hat{\theta}$  as  $r \nabla \theta$

$$(\nabla \times r B_\theta \nabla \theta)_z = \frac{4\pi}{c} J_z$$

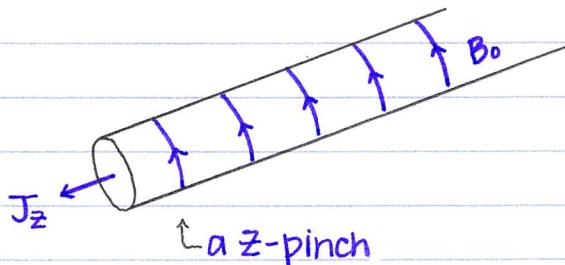
$\nabla \times \nabla \theta = 0$ , so we no longer have to take the curl of this

$$[\nabla(r B_\theta) \times \nabla \theta]_z = \frac{4\pi}{c} J_z$$

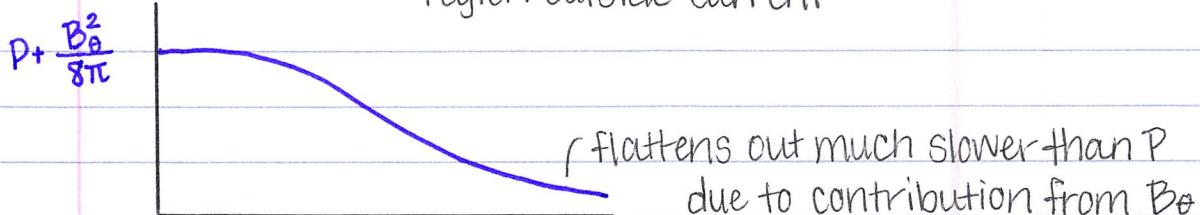
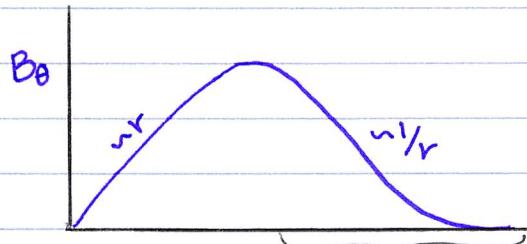
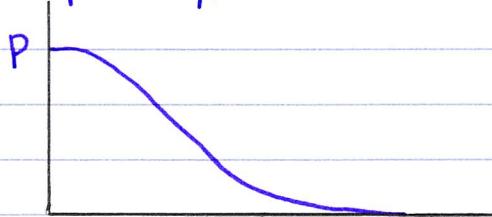
$$\frac{\partial}{\partial r} (r B_\theta) \stackrel{!}{=} \frac{1}{r}$$

$$\Rightarrow \frac{1}{r} \frac{\partial}{\partial r} r B_\theta = \frac{4\pi}{c} J_z$$

What does this look like?



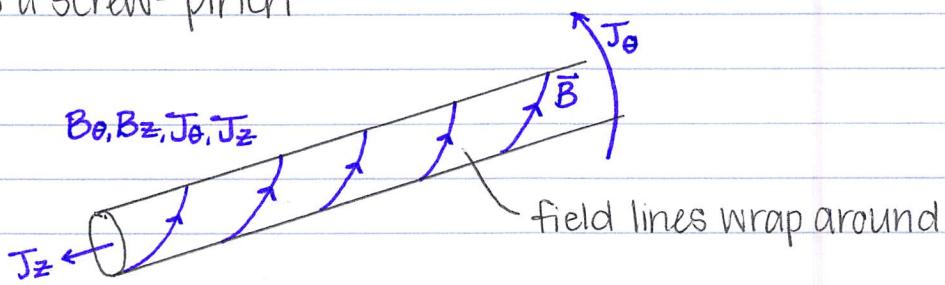
Graphically,



Experiments with both  $B_\theta, B_z \neq 0$  are called screw-pinches.

↳ having  $B_\theta$  &  $B_z$  produces  $J_\theta$  &  $J_z$

\* Magnetic reconnection in the solar corona may be modeled as a screw-pinch



\*\* If you bend this into a torus,  
really crazy stuff happens!