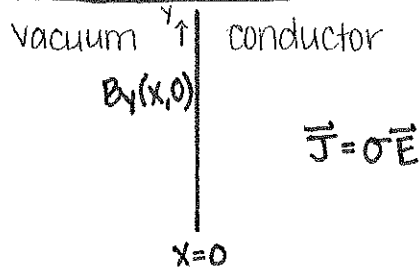


Lecture 14 - Applications of Changing Magnetic Fields

03/22/16

1. The Skin Effect
2. Magnetic Dynamo (Faraday's Law)
3. Displacement Current
4. Scalar and Vector Potentials

1. The Skin Effect



- combine Faraday's, Ampere's, and Ohm's Laws

$$\frac{\partial \vec{B}}{\partial t} = -\nabla \times \vec{E}, \quad \vec{J} = \frac{1}{\mu_0} \nabla \times \vec{B}, \quad \vec{J} = \sigma \vec{E}$$

Together, these yield the diffusion equation

$$\frac{\partial \vec{B}}{\partial t} = \left(\frac{1}{\mu_0 \sigma} \right) \nabla^2 \vec{B}$$

↑ the effective diffusion coefficient

$$d^2 \propto \frac{1}{\mu_0 \sigma} t$$

↳ d = depth of penetration (in skin)

for the above geometry:

$$\vec{B} = \hat{y} B_y(x,t)$$

$$B_y(x,t) = \text{Re} \{ \hat{B}_y(x) e^{-i\omega t} \}$$

↓ apply the diffusion equation ↓

$$\frac{d^2}{dx^2} \hat{B}_y(x) = -i\omega \mu_0 \sigma \hat{B}_y(x)$$

$$\rightarrow \hat{B}_y(x) = \exp(-ikx)$$

choose the solution such that $\text{Re}\{ik\} > 0 \rightarrow$ prevents blow-up at origin

$$k^2 = -i\omega \mu_0 \sigma$$

$$\rightarrow k = \pm \{ \sqrt{-i} \sqrt{\omega \mu_0 \sigma} \}$$

$$\sqrt{-i} = \frac{1-i}{\sqrt{2}}$$

Apply constraints on k_2

$$k = (1-i) \sqrt{\frac{\omega \mu_0 \sigma}{2}}$$

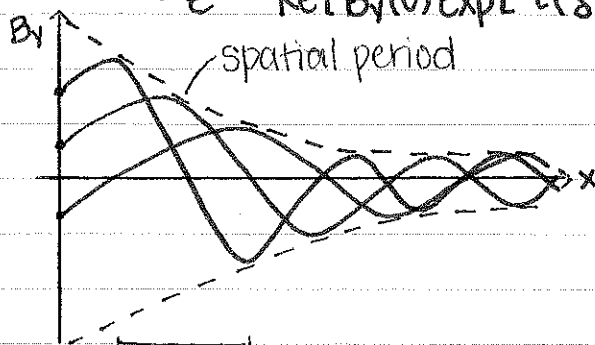
$$\delta = \text{skin depth} = \sqrt{\frac{2}{\omega \mu_0 \sigma}}$$

We can use this to now write:

$$B_y(x,t) = \text{Re} \{ \hat{B}_y(0) \exp[-i\omega t - (1-i)x/\delta] \}$$

creates an envelope of $e^{-x/\delta}$

$$= e^{-x/\delta} \text{Re} \{ \hat{B}_y(0) \exp[-i(\frac{x}{\delta} - \omega t)] \}$$



δ determines the attenuation rate.

$2\pi\delta$, the approximate distance between peaks
(changes slightly due to attenuation)

What about the other fields?

$$B_y = \mu H_y, \quad J_z = \frac{\partial}{\partial x} H_y, \quad E_z = \frac{1}{\sigma} J_z$$

$$\vec{E}_z(x,t) = \text{Re} \{ \hat{E}_z(0) \exp[-i\omega t - (1-i)x/\delta] \}$$

$$\hat{E}_z(0) \left[\frac{V}{m} \right] = - \frac{(1-i)}{\sigma \delta}$$

$\equiv$ Surface impedance

The impedance of a layer
of thickness δ

$$Z_s = \frac{(1-i)}{\sigma \delta}$$

We can now completely characterize conductors
using surface impedance!

Some numbers:

Material	Conductivity	Skin Depth at...		
		60 Hz	1 MHz	1 GHz
Copper	$5.8 \times 10^7 \text{ S/m}$	8.53 mm	0.066 mm	0.0021 mm
Sea Water	4 S/m	32 m	0.25 m	—

polarization & displacement current larger than conduction current here

Power flow is given by the Poynting Flux

$$\vec{S} = \vec{E} \times \vec{H}$$

↳ we will return to this

Surface impedance (Alternate form)

impedance of free space $\sim 377 \Omega$

$$Z_s = \frac{1-i}{2} \sqrt{\frac{\mu_0}{\epsilon_0}} \frac{\omega \delta}{c}$$

$$= \frac{2\pi\delta}{\lambda} \ll 1$$

↳ the vacuum wavelength

from this we can see that surface impedance $\ll$ free space impedance for a conductor.

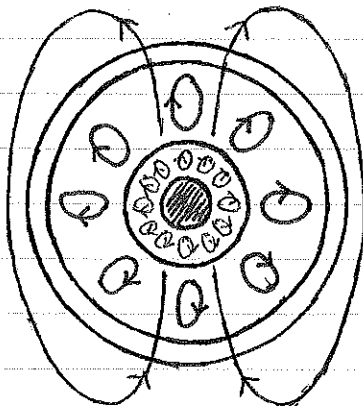
2. Magnetic Dynamo

The conductor is now moving!

↳ we now consider velocity effects

$$\frac{\partial \vec{B}}{\partial t} = -\nabla \times \vec{E}, \quad \vec{J} = \frac{1}{\mu_0} \nabla \times \vec{B}, \quad \vec{J} = \sigma (\vec{E} + \underline{\underline{\vec{v} \times \vec{B}}})$$

The Dynamo explains why Earth_⊕ has a magnetic field.



If you start with a magnetic field already present:

$$d^2 = \mu_0 \sigma t, \quad d = R_{\oplus}$$

$$t = \text{decay time} \approx \underline{15 \text{ kyr}}$$

less than the age of the Earth!

→ this must not be the whole story...

A dynamo allows us to show that even if we start with no $\vec{B}$ -field, one will build up & sustain due to convection.

With a weak starting $\vec{B}$ -field (weak as not to influence flow)...

The kinematic dynamo $\rightarrow$ Does the magnetic field grow or decay in time? (i.e., is no $\vec{B}$ -field stable?)

$\rightarrow$ combining our equations $\rightarrow$

$$\frac{\partial \vec{B}}{\partial t} = -\nabla \times \frac{1}{\sigma \mu_0} (\nabla \times \vec{B}) + \underbrace{\nabla \times (\vec{v} \times \vec{B})}_{=0 \text{ by definition}}$$

$$= \vec{B} \cdot \nabla \vec{v} + (\nabla \cdot \vec{B}) \vec{v} - \vec{v} \cdot \nabla \vec{B} - \underbrace{\vec{B} \nabla \cdot \vec{v}}_{=0}$$

$\rightarrow$ the flow is
INCOMPRESSIBLE

Aside: Continuity of Materials

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) = 0$$

$$\frac{\partial \rho}{\partial t} + \vec{v} \cdot \nabla \rho + \rho \nabla \cdot \vec{v} = 0$$

this is a convective derivative $\rightarrow$ the rate of change of ρ if you move along the medium (move with a fluid element)

$$\frac{d\rho}{dt} = \frac{\partial \rho}{\partial t} + \underbrace{\vec{v} \cdot \nabla \rho}_{d\vec{x}/dt} \text{ must} = 0$$

If you're following a fluid element, this states that you cannot compress the flow.

$$\frac{\partial \vec{B}}{\partial t} = \frac{1}{\sigma \mu_0} \nabla^2 \vec{B}$$

$\rightarrow$ plugging in $\rightarrow$

$$\frac{\partial \vec{B}}{\partial t} + \vec{v} \cdot \nabla \vec{B} = \vec{B} \cdot \nabla \vec{v} + \underbrace{\frac{1}{\mu_0 \sigma} \nabla^2 \vec{B}}_{\text{diffusion of } \vec{B} \text{ due to resistivity}}$$

the change in $\vec{B}$
while following the
rate of flow

typically a damping term

$\rightarrow$ The solution must be dependent on this term concerning the non-uniformity of $\vec{v}$

Suppose $\vec{v} = \text{constant}$

$$\vec{B} \cdot \nabla \vec{v} = 0$$

$$\frac{\partial \vec{B}}{\partial t} + \vec{v} \cdot \nabla \vec{B} = \frac{1}{\mu\sigma} \nabla^2 \vec{B}$$

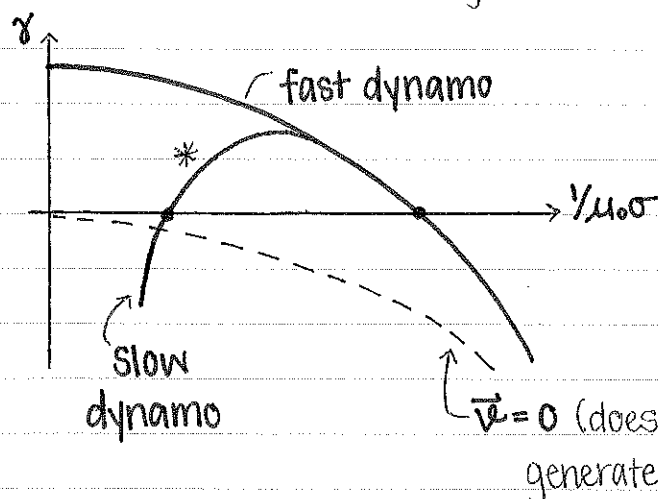
solution of the form:

$$(\gamma + i\vec{k} \cdot \vec{v}) = \frac{-k^2}{\mu\sigma}$$

the Doppler shift! This gives the frequency of decay (damping rate)

$$\gamma = -i\vec{k} \cdot \vec{v} - \frac{k^2}{\mu\sigma}, \text{ a non-additive term!}$$

γ must be > 0 for field growth



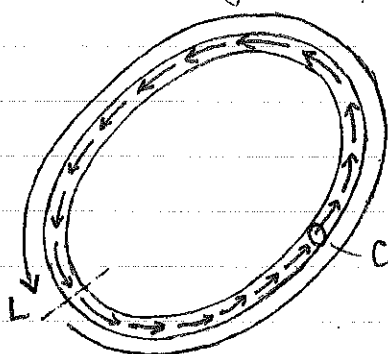
* in the slow dynamo, there is a range of conductivities that allow for growth

Effects of $\vec{v}$: What kind of $\vec{v}(\vec{x}, t)$ is needed?

$\vec{v}(\vec{x}, t)$ should cause

- stretching
- twisting
- folding

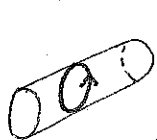
then $\vec{B}$ can grow exponentially



For a tube of fluid, length L

→ Amount of flux passing through A :

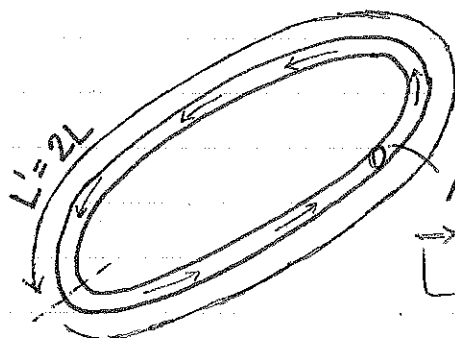
$$\Psi = \int dA \hat{n} \cdot \vec{B}$$



$$\oint (\vec{E} + \vec{v} \times \vec{B}) \cdot d\vec{e} = 0$$

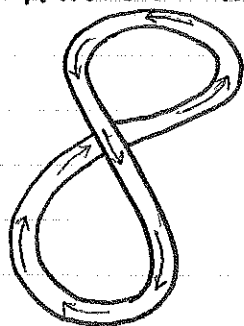
i.e., the conductivity is large enough that the loop of integration is moving with $\vec{B}$, so this never changes.

① $\vec{v}$ stretches the loop



due to incompressibility
 $A' = A/2$
 $\rightarrow \psi' = \psi$, required ($V = A'L' = AL = \text{constant}$)
 $\rightarrow$ the $\vec{B}$ -field must have doubled when the loop was stretched! $B' = 2B$

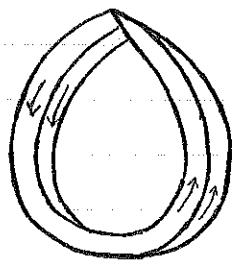
② $\vec{v}$ twists the loop



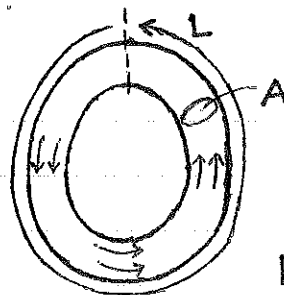
L' and A' unchanged
 $\Rightarrow \psi' = \psi$, $B' = 2B$ (still)

③ $\vec{v}$ folds the loop

Arrows of fluid flow in the twist will align!



$\rightarrow$ apply diffusion $\rightarrow$



$$\psi''' = 2\psi$$

$$B' = 2B (!)$$

We have returned to our original geometry, but our magnetic field has doubled!

$\rightarrow$ this is how stretching, twisting, and folding allow $\vec{B}$ to grow exponentially in time.

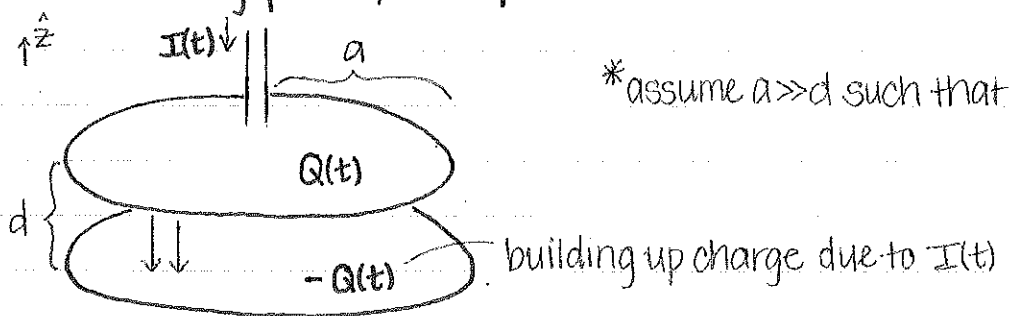


3. Displacement Current

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} ; \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0} ; \nabla \cdot \vec{B} = 0 ; \nabla \times \vec{B} = \mu_0 \left(\vec{J} + \frac{\partial}{\partial t} \epsilon_0 \vec{E} \right)$$

displacement "current"
needed to satisfy
continuity of charge

ex. Conducing plates, fed by I :



For the electrostatic condition, we have

$$E_z(r, t), B_\theta(r, t)$$

- apply Ampere's Law with Displacement Current

$$(\nabla \times \vec{B})_z = \mu_0 \epsilon_0 \frac{\partial E_z}{\partial t}$$

$$\frac{1}{r} \frac{\partial}{\partial r} r B_\theta = \mu_0 \epsilon_0 \frac{\partial E_z}{\partial t}$$

$$= \text{a constant}, E_z(r, t) = E_z(0, t)$$

$$B_\theta(r, t) = \frac{r}{2} \epsilon_0 \mu_0 \frac{\partial E_z}{\partial t}$$

We can now apply Faraday's Law using the approximation of B_θ in the case that $E_z = \text{constant}$

$$-\frac{\partial B_\theta}{\partial t} = (\nabla \times \vec{E})$$

$$= -\frac{\partial}{\partial r} E_z \text{ (for statics)}$$

$$E_z(r) = E_z(0) + \int_0^r dr' \frac{\partial}{\partial t} B_\theta(r', t)$$

$$= E_z(0, t) + \int_0^r dr' \frac{r'}{2} \epsilon_0 \mu_0 \frac{\partial^2}{\partial t^2} E_z(0, t)$$

$$= E_z(0, t) + \underbrace{\epsilon_0 \mu_0 \frac{r^2}{4} \frac{\partial^2}{\partial t^2} E_z(0, t)}_{\text{correction term to the static condition}}$$

correction term to the static condition

$$E_z(r) = E_0 \left(1 - \frac{\omega^2 r^2}{4} \underbrace{\epsilon_0 \mu_0}_{f = \omega/2\pi} \right), \text{ minimum @ } r = a$$

$$\epsilon_0 \mu_0 = \frac{1}{c^2}, \quad \lambda = c/f$$

→ From this we know that statics applies for

$$\frac{1}{4} \omega^2 a^2 \epsilon_0 \mu_0 \ll 1$$

$= \left(\frac{\pi a}{\lambda} \right)^2 \ll 1 \rightarrow$ the static approximation is valid when your wavelength is large compared to the radius of your conductor

What if we did not start with the static condition?

$$\frac{1}{r} \frac{\partial}{\partial r} r B_\theta = \mu_0 \epsilon_0 \frac{\partial}{\partial t} E_z(r, t); \quad \frac{\partial B_\theta}{\partial r} = \frac{\partial}{\partial r} E_z(r, t)$$

↓ combining for an equation purely in E_z ↓

yields the wave equation in 2D cylindrical coordinates

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial E_z}{\partial r} = \epsilon_0 \mu_0 \frac{\partial^2 E_z}{\partial t^2}$$

- assume sinusoidal oscillations

$$E_z(r, t) = \text{Re} \{ \hat{E}_z(r) e^{-i\omega t} \}$$

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \hat{E}_z(r)}{\partial r} + \frac{\omega^2}{c^2} \hat{E}_z(r) = 0 \rightarrow \text{the Bessel function (with dependence on } \omega)$$

Solutions of the form:

$$E_z(r) = E_0 J_0 \left(\frac{\omega}{c} r \right)$$

(bessel)₀ function

$$\frac{1}{x} \frac{\partial}{\partial x} + \frac{\partial}{\partial x} J_0(x) + J_0(x) = 0$$

$$J_0(x) = \sum_{m=0}^{\infty} \frac{(-1)^m (x/2)^{2m}}{(m!)^2}$$

↳ where for small x , we may expand →

$$\approx 1 - \frac{1}{4}x^2 + \mathcal{O}(x^4)$$

the correction term we found!

4. Scalar & Vector Potentials

$$\nabla \cdot \vec{B} = 0, \quad \vec{B} = \nabla \times \vec{A}(\vec{x}, t)$$

$\vec{B}$ must be the curl of $\vec{A}(\vec{x}, t)$, where $\vec{A}$ is a 3-dimensional vector

$$\vec{A} = \begin{pmatrix} A_x(\vec{x}, t) \\ A_y(\vec{x}, t) \\ A_z(\vec{x}, t) \end{pmatrix} \Rightarrow 3 \text{ independent functions}$$

but since $\nabla \cdot \vec{B} = 0$, $\vec{B}$ can only have 2 independent functions

So if we have $B_x(\vec{x}, t)$, $B_y(\vec{x}, t)$

$$B_z = - \left[\frac{\partial}{\partial x} B_y - \frac{\partial}{\partial y} B_x \right]$$

This disparity in the number of independent functions means we can make up a scalar rule about $\vec{A}$

$\Rightarrow$ This is the origin of the Gauge Condition

$$\nabla \times \vec{E} = - \frac{\partial}{\partial t} \nabla \times \vec{A} \rightarrow \nabla \times \left(\vec{E} + \frac{\partial \vec{A}}{\partial t} \right) = 0$$

$$\therefore \vec{E} + \frac{\partial \vec{A}}{\partial t} = - \nabla \phi \rightarrow \vec{E} = - \frac{\partial \vec{A}}{\partial t} - \nabla \phi$$

We must still satisfy Poisson & Ampere's Laws

$$\left. \begin{aligned} P: \nabla^2 \phi + \frac{\partial}{\partial t} \nabla \cdot \vec{A} &= -\rho / \epsilon_0 \\ A: \nabla^2 \vec{A} - \frac{1}{c^2} \frac{\partial^2 \vec{A}}{\partial t^2} - \nabla (\nabla \cdot \vec{A} + \frac{1}{c^2} \frac{\partial \phi}{\partial t}) &= -\mu_0 \vec{J} \end{aligned} \right\} \text{coupled equations}$$

Choices for our scalar rule on $\vec{A}$: *must be wary of causality here

① $\nabla \cdot \vec{A} = 0$, Coulomb's Gauge

$$\text{Where } \phi(\vec{x}, t) = \frac{1}{4\pi\epsilon_0} \int \frac{d^3x' \rho(\vec{x}', t)}{|\vec{x} - \vec{x}'|}$$

② $\phi(x, t) = 0 \rightarrow \vec{E} = - \partial \vec{A} / \partial t$

③ $\nabla_1 \cdot \vec{A} = 0$

④ $\nabla^2 \phi - \frac{1}{c^2} \frac{\partial^2 \phi}{\partial t^2} = -\frac{\rho}{\epsilon_0}$, Lorentz Gauge

$\rightarrow$ causes scalar & vector potentials to be independent