

The Fluid equations Bellen 2.4 - 2.5

The Vlasov equation with a collision operator can describe the dynamics of a plasma from the collisionless limit, all the way to a system with a very high collision rate as long as the plasma parameter Γ is small. In the limit of large collisions we **expect** the dynamics to be fluid-like. Even in the limit of weak collisions fluid like concepts can help to ~~explain~~ understand how a plasma ~~reacts~~ behaves.

We will therefore proceed to construct a set of fluid equations by taking moments of the VE. We will be careful to include collisions so we start with the VE with a collision operator.

$$\frac{\partial}{\partial t} f_\alpha + \mathbf{v} \cdot \nabla f_\alpha + \frac{F_\alpha}{m_\alpha} \cdot \frac{\partial}{\partial \mathbf{v}} f_\alpha = \sum_B C_{\alpha B} f_\alpha$$

$C_{\alpha B}$ = collisions acting on α due to species B.

zero moment

First integrate over the velocity and use fact that $\frac{\partial}{\partial \mathbf{v}} \cdot \mathbf{F} = 0$ and that collisions don't create or destroy particles

$$\sum_B \int \mathbf{v} \cdot \nabla_{\mathbf{v}} C_{\alpha B} f_\alpha = 0$$

and $f_\alpha \rightarrow 0$ as $v \rightarrow \infty$.

$$\frac{\partial}{\partial t} \int d\mathbf{v} f_\alpha + \nabla \cdot \int d\mathbf{v} \mathbf{v} f_\alpha = 0$$

$$\Rightarrow \boxed{\frac{\partial n_\alpha}{\partial t} + \nabla \cdot n_\alpha \mathbf{u}_\alpha = 0} \quad \begin{array}{l} \text{Continuity} \\ \text{Eqs.} \end{array}$$

$$n_\alpha \equiv \int d\mathbf{v} f_\alpha$$

$$n_\alpha \mathbf{u}_\alpha \equiv \int d\mathbf{v} \mathbf{v} f_\alpha \Rightarrow \text{defines } \mathbf{u}_\alpha$$

change in ^{density} number of particles at a location arises from the flux of particles in or out of the region.

First moment

Multiply the VE by \mathbf{v} and integrate. Note the \mathbf{v} is an independent variable so passes through $\nabla, \partial/\partial t$ operators.

$$\frac{\partial}{\partial t} \int d\mathbf{v} f_\alpha \mathbf{v} + \nabla \cdot \int d\mathbf{v} \mathbf{v} \mathbf{v} f_\alpha - \int d\mathbf{v} \left[\frac{\mathbf{F}}{m_\alpha} \cdot \frac{\partial}{\partial \mathbf{v}} \mathbf{v} \right] f_\alpha = - \frac{1}{m_\alpha} R_{\alpha\beta}$$

$$\frac{\partial}{\partial \mathbf{v}} \mathbf{v} = \hat{e}_i \hat{e}_j \frac{\partial}{\partial v_i} v_j = \hat{e}_i \hat{e}_j \delta_{ij} = \frac{\mathbf{I}}{v}$$

$R_{\alpha\beta}$ = drag between species α and β

$R_{\alpha\alpha} = 0$ since within a species no drag

Generally $R_{ei} = v_{ei} m_e n_e (u_e - u_i)$

$R_{ie} = v_{ie} m_i n_i (u_i - u_e)$

$R_{ei} + R_{ie} = 0$

⇒ total momentum of plasma is conserved by collisions.

$\frac{\partial}{\partial t} n_\alpha u_\alpha + \nabla \cdot \underbrace{\sum_n v_n v_n f_n}_{\text{flux of momentum}} - \underbrace{\frac{\partial}{\partial x} n_\alpha \left(E + \frac{1}{c} u_\alpha \times B \right)}_{\text{change of momentum from E field}}$

$= - \frac{1}{m_\alpha} R_{\alpha \beta}$
momentum transfer to other species

Can ~~not~~ extract average velocity from integral

$v = u_\alpha + v'$

and note that $\sum_n v_n v' v' f_n = 0$

$\nabla \cdot \sum_n v_n v_n f_n = \nabla \cdot n_\alpha u_\alpha u_\alpha + \sum_n v_n v' v' f_n$

Define the pressure tensor

$P_\alpha = m_\alpha \sum_n v_n v' v' f_n$

$m_\alpha \left(\frac{\partial}{\partial t} n_\alpha u_\alpha + \nabla \cdot n_\alpha u_\alpha u_\alpha \right) = n_\alpha q_\alpha \left(E + \frac{1}{c} u_\alpha \times B \right) - \nabla \cdot P_\alpha - R_{\alpha \beta}$

Use the continuity eqn to ~~extract~~ extract n_α from the momentum eqn.

$$n_\alpha m_\alpha \left(\frac{\partial}{\partial t} \underline{u}_\alpha + \underline{u}_\alpha \cdot \nabla \underline{u}_\alpha \right) = n_\alpha q_\alpha \left(\underline{E} + \frac{1}{c} \underline{u}_\alpha \times \underline{B} \right) - \nabla \cdot \underline{P}_\alpha - \underline{R}_\alpha$$

This is the fluid momentum equation. Note that it is not complete since it depends on the unknown momentum tensor \underline{P}_α .

General pattern

$$\frac{\partial n_\alpha}{\partial t} + \nabla \cdot n_\alpha \underline{u}_\alpha = 0$$

$$\frac{\partial}{\partial t} m_\alpha n_\alpha \underline{u}_\alpha + () + \nabla \cdot \underline{P}_\alpha = ()$$

$$\frac{\partial}{\partial t} \underline{P}_\alpha + () + \nabla \cdot \text{third moment} = ()$$

\Rightarrow no closure of equations.

Closure with collisions

We know that collisions drive f_α toward a Maxwellian distribution. Thus if collisions are ~~the~~ strong we expect.

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$$f_{\alpha} = \frac{n_{\alpha}}{(2\pi T_{\alpha}/m_{\alpha})^{3/2}} e^{-\frac{(v_x - U_{\alpha})^2 m_{\alpha}}{2T_{\alpha}}} + \delta f_{\alpha}$$

where $\delta f_{\alpha} \sim \frac{1}{V} \Rightarrow$ small

$$P_{\alpha ij} \approx m_{\alpha} \int d^3v' \frac{v_i' v_j'}{m} e^{-\frac{v'^2 m_{\alpha}}{2T_{\alpha}}} \frac{n_{\alpha}}{(2\pi T_{\alpha}/m_{\alpha})^{3/2}}$$

$\Rightarrow P_{\alpha ij}$ is diagonal

\Rightarrow diagonal terms equal

$$P_{\alpha ii} = m_{\alpha} \int d^3v' \frac{v_i'^2}{m} e^{-\frac{v_i'^2 m_{\alpha}}{2T_{\alpha}}} \frac{n_{\alpha}}{(2\pi T_{\alpha}/m_{\alpha})^{3/2}}$$

$$s^2 = \frac{v_i'^2 m_{\alpha}}{2T_{\alpha}}$$

$$P_{\alpha ii} = m_{\alpha} n_{\alpha} \left(\frac{2T_{\alpha}}{m_{\alpha}}\right)^{3/2} \frac{1}{(2\pi T_{\alpha}/m_{\alpha})^{3/2}} \int_{-\infty}^{\infty} ds s^2 e^{-s^2}$$

$$\begin{aligned} \int_{-\infty}^{\infty} ds s^2 e^{-s^2} &= -\frac{d}{ds} \int ds e^{-s^2} = -\frac{d}{ds} \frac{1}{\sqrt{\pi}} \int dp e^{-p^2} \\ &= \frac{\sqrt{\pi}}{2} \end{aligned}$$

$$P_{\alpha ii} = n_{\alpha} T_{\alpha} = P_{\alpha}$$

$$\nabla_{\parallel} P_{\alpha} = \nabla P_{\alpha} + \nabla_{\parallel} S P_{\alpha}$$

$$n_{\alpha} m_{\alpha} \left(\frac{\partial}{\partial t} \underline{u}_{\alpha} + \underline{u}_{\alpha} \cdot \nabla \underline{u}_{\alpha} \right) = n_{\alpha} q_{\alpha} \left(\underline{E} + \frac{1}{c} \underline{u}_{\alpha} \times \underline{B} \right) - \nabla P_{\alpha} - \nabla \cdot \underline{\underline{S}} P_{\alpha} - \underline{R}_{\alpha \beta}$$


 VISCOUS STRESS

Second Moment \Rightarrow energy equation

Multiply VE by $\frac{1}{2} m_{\alpha} v^2$

$$\begin{aligned} \frac{\partial}{\partial t} \int d\underline{v} \frac{m_{\alpha} v^2}{2} f_{\alpha} + \nabla \cdot \left(\int d\underline{v} \frac{m_{\alpha} v^2}{2} \underline{v} f_{\alpha} \right) \\ + q_{\alpha} \int d\underline{v} \frac{v^2}{2} \frac{\partial}{\partial \underline{v}} \cdot \left(\underline{E} + \frac{1}{c} \underline{v} \times \underline{B} \right) f_{\alpha} \\ = \sum_{\beta} \int d\underline{v} \frac{m_{\alpha} v^2}{2} C_{\alpha\beta}(f_{\alpha}) \end{aligned}$$

Again write $\underline{v} = \underline{u}_{\alpha} + \underline{v}'$

$$\begin{aligned} \int d\underline{v} \frac{m_{\alpha} v^2}{2} f_{\alpha} &= \frac{1}{2} m_{\alpha} u_{\alpha}^2 + \int d\underline{v} \frac{m_{\alpha} v'^2}{2} f_{\alpha} \\ &= \frac{1}{2} m_{\alpha} u_{\alpha}^2 + \frac{3}{2} n_{\alpha} T_{\alpha} \end{aligned}$$

$$\begin{aligned} \int d\underline{v} \frac{m_{\alpha} v^2}{2} \underline{v} f_{\alpha} &= \frac{1}{2} m_{\alpha} u_{\alpha}^2 \underline{u}_{\alpha} n_{\alpha} + \int d\underline{v}' \frac{m_{\alpha} v'^2}{2} \underline{v}' f_{\alpha} \\ &+ \int d\underline{v}' \frac{1}{2} m_{\alpha} v'^2 \underline{u}_{\alpha} f_{\alpha} + \int d\underline{v}' \frac{1}{2} m_{\alpha} 2 \underline{v}' \cdot \underline{u}_{\alpha} \underline{v}' f_{\alpha} \end{aligned}$$

$$= \frac{1}{2} m_\alpha u_\alpha^2 u_\alpha n_\alpha + \frac{3}{2} P_\alpha u_\alpha + P_\alpha u_\alpha + Q_\alpha$$

$$Q_\alpha = \int d\mathbf{v}' \frac{m_\alpha v'^2}{2} \mathbf{v}' f_\alpha$$

$$= \frac{1}{2} m_\alpha u_\alpha^2 u_\alpha n_\alpha + \frac{5}{2} P_\alpha u_\alpha + \underbrace{Q_\alpha}_{\text{heat flux}} \sim \frac{1}{v}$$

$$\partial_\alpha \int d\mathbf{v} \frac{v^2}{2} \frac{\partial}{\partial \mathbf{v}} \cdot \left(\mathbf{E} + \frac{1}{c} \mathbf{v} \times \mathbf{B} \right) f_\alpha$$

$$= - \int d\mathbf{v} \mathbf{v} \cdot \left(\mathbf{E} + \frac{1}{c} \mathbf{v} \times \mathbf{B} \right) f_\alpha \partial_\alpha$$

$$= \cancel{\partial_\alpha \int d\mathbf{v} \frac{v^2}{2} f_\alpha} - \partial_\alpha \mathbf{E} \cdot u_\alpha n_\alpha$$

Putting it all together,

$$\frac{\partial}{\partial t} \left(\frac{1}{2} m_\alpha u_\alpha^2 + \frac{3}{2} n_\alpha T_\alpha \right) + \nabla \cdot \left(\frac{1}{2} m_\alpha u_\alpha^2 u_\alpha n_\alpha + \frac{5}{2} P_\alpha u_\alpha + Q_\alpha \right)$$

$$= \partial_\alpha u_\alpha u_\alpha \cdot \mathbf{E} - \underbrace{\left(\frac{\partial W}{\partial t} \right)_{\alpha\beta}}_{\text{rate energy transfer from } \alpha \text{ to } \beta}$$

Note that $\left(\frac{\partial W}{\partial t} \right)_{\alpha\beta} = - \left(\frac{\partial W}{\partial t} \right)_{\beta\alpha}$
 and $\left(\frac{\partial W}{\partial t} \right)_{\alpha\alpha} = 0$

⇒ collisions conserve total energy

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Can simplify by using continuity and momentum equations.

$$\begin{aligned} \frac{3}{2} \left(\frac{\partial}{\partial t} + \underline{u}_\alpha \cdot \nabla \right) P_\alpha + \frac{5}{2} P_\alpha \nabla \cdot \underline{u}_\alpha \\ = - \nabla \cdot \underline{Q}_\alpha + R_{\alpha\beta} \cdot \underline{u}_\alpha - \left(\frac{\partial W}{\partial t} \right)_{\alpha\beta} \end{aligned}$$

In a 3-D system $\frac{3}{2} P_\alpha$ is the internal energy.

$R_{\alpha\beta} \cdot \underline{u}_\alpha$ is frictional heating of α due to drag with β .

Can also consider systems with other degrees of freedom.

$$3 \rightarrow n_f$$

$$5 \rightarrow 2 + n_f$$

$$\begin{aligned} \frac{n_f}{2} \left(\frac{\partial}{\partial t} + \underline{u}_\alpha \cdot \nabla \right) P_\alpha + \frac{n_f + 2}{2} P_\alpha \nabla \cdot \underline{u}_\alpha \\ = - \nabla \cdot \underline{Q}_\alpha + R_{\alpha\beta} \cdot \underline{u}_\alpha - \left(\frac{\partial W}{\partial t} \right)_{\alpha\beta} \end{aligned}$$

No heat flux or collisional heating or energy loss.

⇒ adiabatic

$$\frac{n_e}{2} \left(\frac{d}{dt} + \mathbf{u}_\alpha \cdot \nabla \right) P_\alpha + \frac{n_e + 2}{2} P_\alpha \nabla \cdot \mathbf{u}_\alpha = 0$$

From continuity $\frac{1}{P_\alpha} \frac{d}{dt} P_\alpha + \gamma_s \nabla \cdot \mathbf{u}_\alpha = 0$

$\gamma_s = \frac{n_e + 2}{n_e}$ ratio of specific heats.

$$\frac{d n_\alpha}{dt} + \mathbf{u}_\alpha \cdot \nabla n_\alpha + n_\alpha \nabla \cdot \mathbf{u}_\alpha = 0$$

$$\gamma_s \left(\frac{1}{n_\alpha} \frac{d}{dt} n_\alpha + \nabla \cdot \mathbf{u}_\alpha \right) = 0$$

Subtract equations

~~$$\frac{d}{dt} \frac{d}{dt} P_\alpha = -\gamma_s$$~~

$$\frac{1}{P_\alpha} \frac{d}{dt} P_\alpha = \gamma_s \frac{1}{n_\alpha} \frac{d}{dt} n_\alpha$$

$$\frac{d}{dt} \left(\ln P_\alpha - \ln n_\alpha^{\gamma_s} \right) = 0$$

$$\frac{d}{dt} \left(\frac{P_\alpha}{n_\alpha^{\gamma_s}} \right) = 0$$

⇒ $\frac{P_\alpha}{n_\alpha^{\gamma_s}} = \text{const in frame of moving plasma.}$